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Thermodynamics of paired charge-compensating doped ceria with superior redox performance for solar thermochemical splitting of H₂O and CO₂

Hoes, Marie ; Muhich, Christopher L ; Jacot, Roger ; Patzke, Greta R ; Steinfeld, Aldo

Abstract: Paired charge-compensating doped ceria (PCCD) using trivalent and pentavalent cations are evaluated as redox materials for the thermochemical splitting of H₂O and CO₂. The oxygen nonstoichiometries of PCCD materials with formulas of Ce_{0.9A}0.05Nb_{0.05}O₂ (A = Y, La, Sc) and Ce_xLa_{(1-x)/2}Nb_{(1-x)/2}O₂ (x = 0.75, 0.95) were measured in a thermogravimetric analyzer over a range of temperatures (T = 1173–1773 K) and oxygen partial pressures (pO₂ = 10^{−15}–10^{−1} atm). Undoped and single element doped ceria (Ce_{0.9B}0.1O₂ where B = Y, La, Nb, Hf) served as a reference. At any given set of T and pO₂, the relative reduction extent follows Ce_{0.9Hf}0.1O₂ > Ce_{0.9Sc}0.05Nb_{0.05}O₂ > Ce_{0.9Y}0.05Nb_{0.05}O₂ > Ce_xLa_{(1-x)/2}Nb_{(1-x)/2}O₂ > CeO₂ > solely trivalent or pentavalent doped ceria. The partial molar reduction enthalpies were determined using Van't Hoff analysis coupled to defect modeling and range from 360 to 410 kJ mol^{−1}. A system efficiency model predicts that these PCCD materials have the potential of achieving high solar-to-fuel energy conversion efficiencies because of their balanced reduction and oxidation properties. Ce_{0.9Y}0.05Nb_{0.05}O₂ in particular can outperform undoped ceria and reach efficiency values of 31% and 28% for H₂ and CO production, respectively.

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View Journal | View IssueCite this: *J. Mater. Chem. A*, 2017, 5, 19476Thermodynamics of paired charge-compensating doped ceria with superior redox performance for solar thermochemical splitting of H₂O and CO₂†Marie Hoes,^a Christopher L. Muhich,^a Roger Jacot,^b Greta R. Patzke^b and Aldo Steinfeld^a

Paired charge-compensating doped ceria (PCCD) using trivalent and pentavalent cations are evaluated as redox materials for the thermochemical splitting of H₂O and CO₂. The oxygen nonstoichiometries of PCCD materials with formulas of Ce_{0.9}A_{0.05}Nb_{0.05}O₂ (A = Y, La, Sc) and Ce_xLa_{(1-x)/2}Nb_{(1-x)/2}O₂ (x = 0.75, 0.95) were measured in a thermogravimetric analyzer over a range of temperatures (*T* = 1173–1773 K) and oxygen partial pressures (*p*_{O₂} = 10^{−15}–10^{−1} atm). Undoped and single element doped ceria (Ce_{0.9}B_{0.1}O₂ where B = Y, La, Nb, Hf) served as a reference. At any given set of *T* and *p*_{O₂}, the relative reduction extent follows Ce_{0.9}Hf_{0.1}O₂ > Ce_{0.9}Sc_{0.05}Nb_{0.05}O₂ > Ce_{0.9}Y_{0.05}Nb_{0.05}O₂ > Ce_xLa_{(1-x)/2}Nb_{(1-x)/2}O₂ > CeO₂ > solely trivalent or pentavalent doped ceria. The partial molar reduction enthalpies were determined using Van't Hoff analysis coupled to defect modeling and range from 360 to 410 kJ mol^{−1}. A system efficiency model predicts that these PCCD materials have the potential of achieving high solar-to-fuel energy conversion efficiencies because of their balanced reduction and oxidation properties. Ce_{0.9}Y_{0.05}Nb_{0.05}O₂ in particular can outperform undoped ceria and reach efficiency values of 31% and 28% for H₂ and CO production, respectively.

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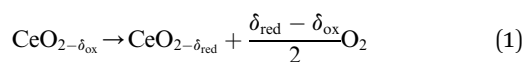
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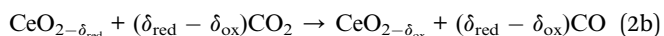
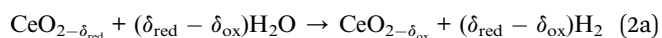
1. Introduction

The thermochemical splitting of H₂O and CO₂ via two-step redox cycles driven by concentrated solar energy is a favorable thermodynamic pathway to produce renewable fuels, because it uses the entire solar spectrum to generate H₂/CO and O₂ in separate steps.^{1–3} Nonstoichiometric ceria has emerged as the benchmark redox material mainly due to its fast kinetics and morphological stability^{4–8} even after hundreds of consecutive redox cycles.⁹ The redox cycle is represented by:

Reduction:



Oxidation:



It consists of an endothermic reduction step (eqn (1)) followed by an exothermic oxidation step with H₂O and CO₂ at lower temperatures (eqn (2a) and (2b), respectively). The difference in the reduction extent, given by the change in the nonstoichiometry $\Delta\delta = \delta_{\text{red}} - \delta_{\text{ox}}$, determines the specific amount of H₂ and CO produced per cycle and mole of ceria, and depends on the reaction temperature (*T*) and the oxygen partial pressure (*p*_{O₂}) of each step. The technical feasibility of this cycle has been experimentally demonstrated with a 5 kW solar reactor, yielding high selectivity, stability, mass conversion and solar-to-fuel energy efficiency.¹⁰ However, due to its relatively low reducibility, pure ceria requires *T* > 1773 K and *p*_{O₂} < 10 mbar to achieve even moderate values of $\Delta\delta$. Doping ceria with tetravalent transition metals such as Zr⁴⁺ (ref. 11–16) and Hf⁴⁺ (ref. 14 and 17) increases $\Delta\delta$ under the same *T* and *p*_{O₂}, while other dopants fail to do so.^{1,11,14,17–25} Hercynite and selected perovskites, e.g. Sr- and Mn-doped LaAlO₃, have lower reduction enthalpies and therefore achieve higher reduction extents,^{26–28} but they suffer from less favorable oxidation thermodynamics, which leads to lower specific fuel yields under most conditions.²⁹ Therefore, the search continues for metal oxides which balance the energetics of reduction and oxidation to yield high solar-to-fuel energy conversion efficiencies.

Density function theory (DFT) simulations suggest that non-reducing tetravalent cations with ionic radii between those of Ti and Ce should be doped into the host lattice of ceria to improve its redox performance.³⁰ No single element other than Zr and Hf

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exists which meets the criteria for improving ceria performance.³¹ Interestingly, by using paired charge-compensating dopants (PCCD), aliovalent cations can be made to mimic tetravalent dopant behavior.³² Specifically, by co-doping ceria with trivalent and pentavalent cations (+3/+5), the trivalent cation exhibits tetravalent like behavior. DFT predicts that the +3/+5 PCCDs have reduction energies between those of pure ceria and Hf/Zr doped ceria, resulting in a desirable trade-off between reducibility and oxidizability. However, a thermodynamic analysis for these promising PCCD redox materials has not been performed to date.

In this work, we thermodynamically characterize $\text{Ce}_{0.9}\text{A}_{0.05}\text{Nb}_{0.05}\text{O}_2$ ($\text{A} = \text{Y}, \text{La}, \text{Sc}$) and $\text{Ce}_x\text{La}_{(1-x)/2}\text{Nb}_{(1-x)/2}\text{O}_2$ ($x = 0.75, 0.95$) and compare their redox performance to undoped and single element doped ceria ($\text{Ce}_{0.9}\text{B}_{0.1}\text{O}_2$ where $\text{B} = \text{Y}, \text{La}, \text{Nb}, \text{Hf}$). We determine their partial molar reduction enthalpies and entropies using a Van't Hoff analysis. The thermodynamic properties are subsequently used in a system efficiency model to calculate the solar-to-fuel energy conversion efficiency.

2. Methods

2.1 Materials synthesis

Powders of $\text{Ce}_{0.9}\text{A}_{0.05}\text{Nb}_{0.05}\text{O}_2$ ($\text{A} = \text{Y}, \text{La}, \text{Sc}$), $\text{Ce}_x\text{La}_{(1-x)/2}\text{Nb}_{(1-x)/2}\text{O}_2$ ($x = 0.75, 0.95$), and $\text{Ce}_{0.9}\text{B}_{0.1}\text{O}_2$ ($\text{B} = \text{Y}, \text{La}, \text{Nb}, \text{Hf}$) were produced by a modified Pechini method.¹⁴ For the sake of clarity, abbreviations are used for the materials according to ABX where A is the first dopant, B is the second dopant and X is the concentration of each dopant, *i.e.* LaNb5 stands for $\text{Ce}_{0.9}\text{La}_{0.05}\text{Nb}_{0.05}\text{O}_2$. For the synthesis of doped ceria samples, citric acid (Sigma-Aldrich, 99%) and the desired metal nitrates or chlorides were dissolved in a 3 : 2 molar ratio in anhydrous ethylene glycol (Sigma-Aldrich, 99.8%) with an approximate citric acid to ethylene glycol mass ratio of 1 : 15. In the case of Hf10, deionized water was used as the solvent. The metal salts used were cerium(III) nitrate hexahydrate (Sigma-Aldrich, 99%), lanthanum(III) nitrate hexahydrate (Alfa Aesar, 99.9%), yttrium(III) nitrate hexahydrate (Strem, 99.5%), scandium(III) nitrate pentahydrate (Strem, 99.5%), niobium(V) chloride (Strem, 99%) and hafnium(IV) chloride (Alfa Aesar, 98%). The mixtures were stirred for 2 hours at 363 K on a magnetic hotplate. The temperature was then gradually increased until the ethylene glycol reaction mixture self-ignited and a powder was formed. The powders were calcined at 1273 K for 1 hour with an initial heating rate of 5 K min⁻¹. Subsequently, the powders were uni-axially cold-pressed under 5 tons into dense cylindrical pellets with a diameter of 8 mm. The pellets were then sintered at 1773 K for 5 hours. The high sintering temperature was used to ensure that the pellet would not melt during cycling and to assess whether the dopant cations segregated at high temperatures.

2.2 Materials characterization

Powder X-ray diffraction (PXRD) was used to determine the phases present and was performed on a STOE STADI P

diffractometer in transmission mode with Cu-K α radiation, a Ge-monochromator, and a Mythen 1K detector. Compositions of all materials were examined by ICP-OES analysis performed on a Icap-6500 Dual View (Thermo Instruments). For ICP-OES analysis, powders of the materials were dissolved for 10 hours in H_2SO_4 followed by hydrolysis with HCl addition. X-ray photoelectron spectroscopy (XPS) was performed on a Phi5000 VersaProbe (ULVAC-PHI, INC.). Spectra were acquired at a base pressure of 5×10^{-8} Pa using a focused scanning monochromatic Al-K α source (1486.6 eV) with a spot size of 200 μm scanning a $500 \times 1000 \mu\text{m}$ area.

Sample surfaces were analyzed before and after thermogravimetric analysis (TGA) by scanning electron microscopy (SEM, Hitachi TM-1000, 15 kV accelerating voltage). The oxygen nonstoichiometry of the materials was measured by thermogravimetric analysis (Setaram Setsys Evolution). The samples, with masses ranging between 220–373 mg, were suspended from the balance with a custom-made platinum hook to eliminate mass transfer limitations. The gas atmosphere in the TGA was controlled by varying the gas flow rates of Ar (Messer, Ar 4.6), O_2/Ar (500 ppm, 0.5 or 50 mol% O_2 balance Ar, Messer, 5.0), CO_2 (Messer, 4.6) and CO/CO_2 (30/70 mol%, Messer 5.0). Gas flows were adjusted using electronic mass flow controllers (Brooks, Model 5850TR, accuracy $\pm 1\%$). Buoyancy effects were accounted for by subtracting a blank run (Al_2O_3 pellet) which was conducted under the same conditions as the measurements. TGA experiments were conducted in the temperature range of $T = 1173\text{--}1773$ K at oxygen partial pressure ranges of $p_{\text{O}_2} = 1.6 \times 10^{-15}\text{--}5.0 \times 10^{-1}$ atm ($T = 1573\text{--}1723$ K and $p_{\text{O}_2} = 10^{-5}\text{--}10^{-2}$ atm for La10, Y10, and Nb10). To determine the reduction extent at a specified T and p_{O_2} , samples were heated to the set point temperatures followed by isothermal reduction and oxidation induced by rapidly changing the p_{O_2} and allowing a new equilibrium state to be reached. In between two measurement temperatures, samples were cooled to 1073 K under the highest p_{O_2} that was used in the respective experiment in order to fully reoxidize it; this point served as a baseline to account for any TGA drift.

2.3 Efficiency model

The solar-to-fuel energy conversion efficiency, $\eta_{\text{solar-to-fuel}}$, is defined as the ratio of the heating value of the fuel produced to the sum of the solar radiative energy input and additional parasitic energy inputs. $\eta_{\text{solar-to-fuel}}$ was calculated for H_2 and CO production with an in-house MATLAB code, following the system efficiency model described by Ehrhart *et al.*³³ This system model accounts for the solar radiative input and heat sinks in an ideal continuous solar reactor under thermodynamic equilibrium, including optical solar concentration losses, re-radiation losses, reduction enthalpies, O_2 removal, solids and gas heating, gaseous product separation, mechanical work, and heat-to-work efficiencies, as well as heat recovery of solids, O_2 , unreacted H_2O and CO_2 , and the exothermic oxidation. The baseline parameters for the efficiency calculation are listed in Table 1.



Table 1 Baseline parameters for the system efficiency model

	CO ₂	H ₂ O
Reduction temperature	1773 K	1773 K
Reduction pressure	1 Pa	1 Pa
Product yield	100%	~100%
Product flow rate	1 mol s ⁻¹	1 mol s ⁻¹
Purity CO, H ₂	0.99	0.999
Product separation temperature	300 K	300 K
Product separation efficiency	0.1	1
Heat recovery gas efficiency	0.9	0.9
Oxygen removal efficiency	0.1	0.1
Mechanical efficiency	0.15	0.15
Optical efficiency	0.9	0.9
Solar concentration ratio	3000	3000
DNI	1 kW m ⁻²	1 kW m ⁻²
Absorptivity	0.95	0.95

3. Experimental results and discussion

3.1 Materials characterization

The fabrication of the PCCD materials was successful as dopant concentrations were within 1 mol% of the nominal values, as determined by ICP-OES. We therefore keep the nominal notation in the following. Targeted elemental concentrations and values measured by ICP-OES are shown in Table 2.

PXRD patterns show that all of the synthesized materials are phase pure and exhibit the fluorite structure in line with undoped ceria. Slight 2θ shifts are attributed to the differences in ionic radii and the resulting slight differences in lattice parameters. The lattice parameters of all materials, calculated based on PXRD patterns, are shown in Table 3. No structural changes were observed after the TGA runs. The PXRD patterns

of YNb5 before and after TG analysis are shown in Fig. 1 along with the PXRD patterns of Hf10, LaNb5, and ScNb5 after TG analysis and a pure ceria reference. All PXRD patterns are shown in Fig. S1 (ESI†). The mean surface oxidation states of Ce, Y, and Nb were estimated by XPS for the YNb5 sample before TG analysis, as well as for the YNb5, Y10 and Nb10 samples after TG. The cerium cations are present in both, 3+ and 4+ oxidation state in all samples which we attributed to the fact that the samples are partly reduced since the XPS analysis is conducted under vacuum. Y cations are present in the only possible oxidized state of 3+. Nb cations, which nominally adopt 2+, 4+ and 5+ oxidation states, exhibit binding energy peaks for energy levels that correspond to an oxidation state of 5+, as shown in Fig. 2. Overall, XPS analysis indicates that Nb and Y behave as 3+/5+ dopants which do not change oxidation states after cycling. In the SEM images taken before and after TG analysis, we observed an increased average grain size and fewer pores due to sintering during TGA experiments, as shown for YNb5 in Fig. 3. Images of all of the materials are shown in Fig. S2 (ESI†).

3.2 Thermogravimetric analysis

The oxygen nonstoichiometries as a function of T and p_{O_2} were determined by TGA. An exemplary set of thermogravimetric measurements in the range $T = 1573$ – 1723 K and $p_{O_2} = 2.5 \times 10^{-5}$ – 2.5×10^{-4} atm is shown in Fig. 4. The mass changes are due to reduction and oxidation, and are calculated relative to the sample mass after stabilization at 1073 K. As the sample is heated from 1073 K to the desired T , the mass decreases and reaches equilibrium, after which p_{O_2} is rapidly altered. Hf doped ceria exhibits the largest mass change followed by the PCCD materials. All TGA measurements are shown in Fig. S3 (ESI†).

The reduction extent is given by: $\Delta\delta = \delta - \delta_{\text{ref}} = \frac{\Delta m}{m_s} \times \frac{M_s}{M_o}$, where Δm is the relative weight loss at equilibrium calculated relative to the stabilization at 1073 K, m_s is the sample mass, M_s is the molar mass of the sample, M_o is the molar mass of atomic oxygen, and δ_{ref} is the nonstoichiometry at $T = 1073$ K and $p_{O_2} = 0.5$ atm. Because of the small Δm induced by altering p_{O_2} in the range 2.5×10^{-4} – 5.0×10^{-1} atm at 1073 K ($\Delta\delta_{\text{ref}} < 0.0011$ for ScNb5; $\Delta\delta_{\text{ref}} < 0.0003$ for the other materials), the sample is assumed to be fully oxidized under these T and p_{O_2} conditions, i.e. $\delta_{\text{ref}} \approx 0$. Thus, we assume that $\Delta\delta = \delta$ except for La10 and Y10 which have a starting nonstoichiometry of $\delta_0 = 0.05$ because trivalent dopants induce one intrinsic oxygen vacancy for every two dopant atoms. For easier comparison, the reduction extents of La10 and Y10 are plotted with a starting reduction extent of zero but the intrinsic oxygen vacancies were considered when fitting the data to a defect model, as discussed later. The reduction extents of all investigated materials are shown in Fig. 5a at $T = 1723$ K and $p_{O_2} = 2.5 \times 10^{-4}$ – 4.8×10^{-3} atm. Similar plots are provided in Fig. S4 (ESI†) for $T = 1173$ – 1773 K and $p_{O_2} = 10^{-15}$ – 10^{-1} atm.

$\Delta\delta$ depends on composition and dopant concentration, with relative reduction extents following the trend $\text{Ce}_{0.9}\text{Hf}_{0.1}\text{O}_2 > \text{Ce}_{0.9}\text{Sc}_{0.05}\text{Nb}_{0.05}\text{O}_2 > \text{Ce}_{0.9}\text{Y}_{0.05}\text{Nb}_{0.05}\text{O}_2 > \text{Ce}_x\text{La}_{(1-x)/2}\text{Nb}_{(1-x)/2}\text{O}_2 > \text{CeO}_2 > \text{Ce}_{0.9}\text{Nb}_{0.1}\text{O}_2 > \text{Ce}_{0.9}\text{La}_{0.1}\text{O}_2 > \text{Ce}_{0.9}\text{Y}_{0.1}\text{O}_2$. The

Table 2 Targeted and measured material compositions of the synthesized materials in mol%

Material	Element	Ce	Hf	La	Y	Sc	Nb
YNb5	Targeted	90.0			5.0		5.0
	Measured	89.6			5.0		5.4
ScNb5	Targeted	90.0				5.0	5.0
	Measured	90.0				4.4	5.5
LaNb5	Targeted	90.0		5.0			5.0
	Measured	89.8		5.1			5.0
LaNb2.5	Targeted	95.0		2.5			2.5
	Measured	95.0		2.5			2.5
LaNb12.5	Targeted	75.0		12.5			12.5
	Measured	75.1		11.5			13.3
Hf10	Targeted	90.0	10.0				
	Measured	90.5	9.5				
La10	Targeted	90.0		10.0			
	Measured	90.0		10.0			
Nb10	Targeted	90.0					10.0
	Measured	89.7					10.3
Y10	Targeted	90.0			10.0		
	Measured	90.2			9.8		



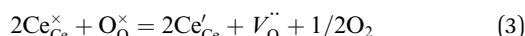
Table 3 Lattice parameters in Å before and after TG analysis. Values are calculated based on PXRD patterns

[Å]	CeO ₂ (ref)	YNb5	ScNb5	LaNb5	LaNb2.5	LaNb12.5	La10	Y10	Nb10	Hf10
Before TGA	5.409	5.412	—	5.421	—	—	5.456	5.416	5.417	5.389
After TGA	5.409	5.411	5.410	5.423	5.424	5.432	5.452	5.415	5.422	5.392

reduction extent of LaNb doped ceria decreases with increasing dopant concentration. However, at 1173 K and 1273 K, the reduction extent of LaNb2.5 is between that of LaNb12.5 and LaNb5, with the caveat that at these temperatures the differences are small.

3.3 Thermodynamic properties

The partial molar enthalpy and entropy are determined to predict the redox performance under conditions other than those experimentally studied. A defect model is employed to interpolate/extrapolate $\delta(T, p_{O_2})$. For small reduction extents, a dilute species behavior is generally assumed^{36–38} and the reduction of pure ceria can be described in Kröger-Vink notation as:³⁷



where $\text{Ce}_{\text{Ce}}^{\times}$ indicates a Ce^{4+} cation on a cerium lattice site, $\text{O}_{\text{O}}^{\times}$ an O^{2-} anion on an oxygen lattice site, Ce_{Ce}' a Ce^{3+} cation on a cerium lattice site and $V_{\text{O}}^{\cdot\cdot}$ a vacancy on an oxygen lattice site that has a 2+ charge to maintain charge neutrality. Here we note just for clarity that no positive charge actually localizes on the O vacancy,³⁹ and the notation is merely a useful charge book-keeping tool. The assumed equilibrium relationship for point defects is:

$$K_1 = \frac{[\text{Ce}_{\text{Ce}}']^2 [V_{\text{O}}^{\cdot\cdot}] p_{\text{O}_2}^{1/2}}{[\text{Ce}_{\text{Ce}}^{\times}]^2 [\text{O}_{\text{O}}^{\times}]} \quad (4)$$

A site balance for cerium and oxygen leads to:

$$\text{Ce}_{\text{Ce}}^{\times} + \text{Ce}_{\text{Ce}}' = 1 - y \quad (5)$$

$$V_{\text{O}}^{\cdot\cdot} = \delta \quad (6)$$

where y is the total dopant concentration. In addition to the site balance, the total charge of the system must remain neutral, and therefore the charge balance depends on the oxidation state of the dopant in addition to the number of vacancies and Ce^{3+} ions. It is written as:

$$\text{Ce}_{\text{Ce}}' + \beta y = 2V_{\text{O}}^{\cdot\cdot} \quad (7)$$

where β equals 1 for trivalent dopants, 0 for tetravalent PCCD materials and -1 for pentavalent dopants. However, the isolated Ce^{3+} and $V_{\text{O}}^{\cdot\cdot}$ model does not adequately describe the

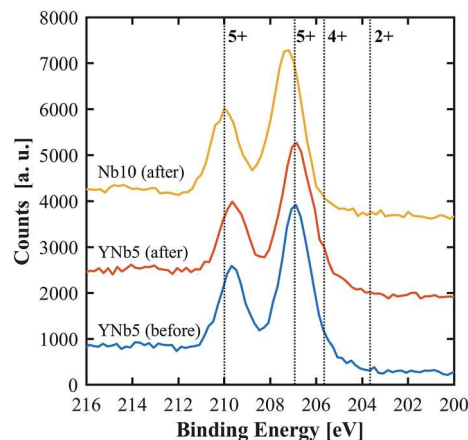


Fig. 2 XPS spectra of Nb 3d for YNb5 before and after TG analysis as well as Nb10 after TG analysis. Reference binding energies (dotted lines) for Nb_2O_5 (5+), NbO_2 (4+) and NbO (2+) were taken from Bahl *et al.*³⁴ and Özer *et al.*³⁵

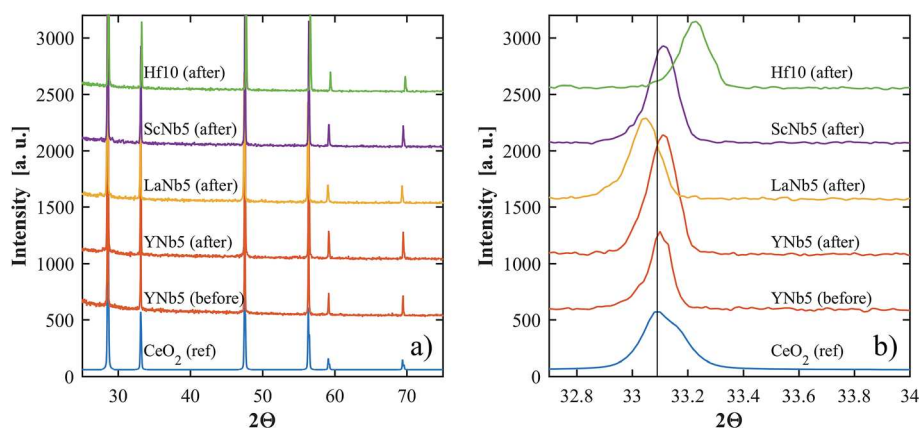


Fig. 1 (a) PXRD patterns of YNb5 before and after TG analysis, and Hf10, LaNb5, and ScNb5 after TG analysis. A reference pattern of undoped ceria is included for comparison. (b) Shows a close up of the peaks around 33.1°.



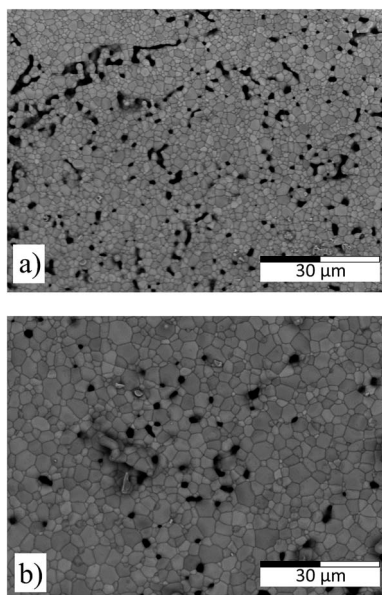
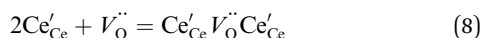


Fig. 3 SEM images of the YNb5 sample surface before (a) and after (b) TG analysis.

nonstoichiometry behavior.⁴⁰ The consideration of additional reactions is required, specifically defect species clustering according to:⁴¹



resulting in two equilibrium constants:

$$K_1 = \frac{[2V_{\text{O}}^{\bullet\bullet} - \beta y]^2 [V_{\text{O}}^{\bullet\bullet}] p_{\text{O}_2}^{1/2}}{[1 - 2\delta - y(1 - \beta)]^2 [2 - \delta]} \quad (9)$$

$$K_2 = \frac{[\text{Ce}'_{\text{Ce}} V_{\text{O}}^{\bullet\bullet} \text{Ce}'_{\text{Ce}}]}{[\text{Ce}'_{\text{Ce}}]^2 [V_{\text{O}}^{\bullet\bullet}]} = \frac{\delta - [V_{\text{O}}^{\bullet\bullet}]}{[2V_{\text{O}}^{\bullet\bullet} - \beta y]^2 [V_{\text{O}}^{\bullet\bullet}]} \quad (10)$$

We tested this model by using a least squares method to determine K_1 and K_2 simultaneously for our experimental data. The combination of the point and cluster defect models describes accurately the nonstoichiometry of our materials. K_1 for tetravalent dopants ($\beta = 0$) was used for all materials except Y10 and La10 where the point defect model for trivalent dopants ($\beta = 1$) was used. Although the Nb cations in Nb10 are pentavalent dopants, the pentavalent model did not fit the experimental data; however, the tetravalent model exhibits good agreement to the experimental data. This suggests that the additional electron of Nb does not significantly alter the reduction behavior of ceria. The fit of the defect models to the nonstoichiometry data of the 5 mol% PCCD materials and Hf10 are shown in Fig. 5b–e.

A linear correlation between $\ln(K)$ and $1/T$ is applied to expand the temperature range. We used a least squares approach to linearly fit the isothermally determined equilibrium constants calculated from the experimental data by assuming a constant standard enthalpy change over the investigated temperature range. A comparison of the experimentally

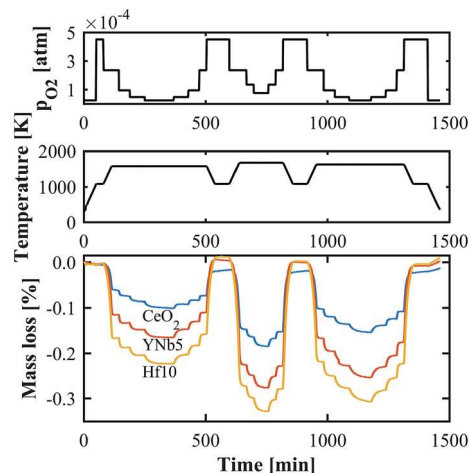


Fig. 4 Exemplary TGA run for CeO₂, YNb5 and Hf10 at $T = 1573\text{--}1723$ K and $p_{\text{O}_2} = 2.5 \times 10^{-5}\text{--}2.5 \times 10^{-4}$ atm.

derived and the fitted equilibrium constants is shown in Fig. 6 for YNb5. All plots are shown in Fig. S5.†

Although fitted and experimentally determined equilibrium constants occasionally differ, we found that the fit to the experimental data is good and the difference in resulting reduction thermodynamics and nonstoichiometries is comparably small. As seen in Fig. 5, the predicted nonstoichiometries based on the fitted equilibrium constants show good agreement with experimental data even when extrapolated to temperatures that were not considered in the fitting process such as $T = 1173$ K, which was explicitly excluded from the Van't Hoff analysis for comparison purposes. By using the fitted equilibrium constants, the influence of random errors is reduced and the extracted data is smoothened. In general, values for K_2 are several orders of magnitude larger than those for K_1 , implying that oxygen vacancies preferentially form defect clusters, as found both experimentally and in atomistic models.^{39,42–45} Only in the case of Hf10, Y10, and ScNb5 are K_2 and K_1 of the same order of magnitude. While these models accurately reproduce the nonstoichiometric data, eqn (9) and (10) do not necessarily represent the reaction mechanism.

The standard Gibbs free energy for the reduction is given by:

$$\Delta_r G^0 = -RT \ln(p_{\text{O}_2}^{\text{eq}}/p^0)^{1/2} \quad (11)$$

assuming unity for the solids activity and ideal gas behavior for oxygen. At constant δ , and further assuming that the thermodynamic properties are independent of temperature in the investigated range, the Gibbs free energy is also given by:

$$\Delta_r G^0 = \overline{G}^0 = \overline{H}^0 - T\overline{S}^0|_{\delta} \quad (12)$$

where G^0 , H^0 and S^0 are the standard partial molar Gibbs free energy, enthalpy and entropy, respectively. Combining eqn (11) and (12) leads to:

$$-\frac{1}{2} \ln(p_{\text{O}_2}^{\text{eq}}/p^0) = \frac{\overline{H}^0}{RT} - \frac{\overline{S}^0}{R}|_{\delta} \quad (13)$$



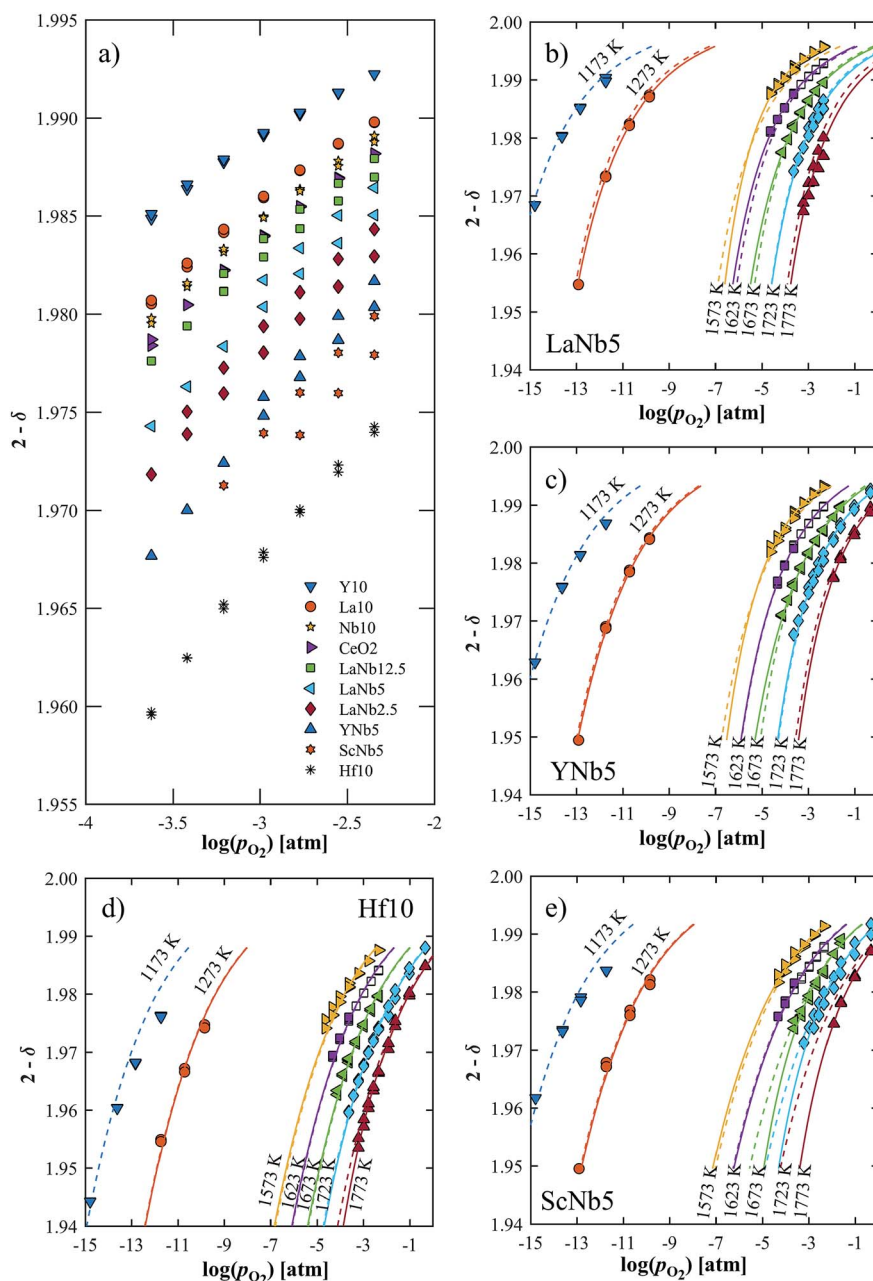


Fig. 5 (a) Oxygen nonstoichiometry at 1723 K in the range $p_{\text{O}_2} = 2.5 \times 10^{-4} - 4.8 \times 10^{-3}$ atm. (b–e) Measured nonstoichiometry (symbols) of (b) LaNb5, (c) YNb5, (d) Hf10 and (e) ScNb5 as a function of $\log(p_{\text{O}_2})$. Closed symbols indicate this work while open symbols are taken from ref. 32. Solid lines show the predicted nonstoichiometry based on isothermally derived equilibrium constants; the dashed lines are based on the inversed temperature dependence of $\ln(K_1)$ and $\ln(K_2)$.

where $p_{\text{O}_2}(T, \delta)$ is obtained from the defect model. H^0 and S^0 were then determined by linear regression from p_{O_2} and $1/T$ at constant δ . An example is shown for YNb5 in Fig. 7 in the ranges $T = 1173\text{--}1723$ K and $\delta = 0.010\text{--}0.032$. The extracted H^0 is plotted in Fig. 8a.

The H^0 's of the PCCD materials are between that of Hf10 and pure ceria, consistent with DFT predictions.³² The PCCD materials exhibit a constant or slightly increasing H^0 with increasing reduction extent. The values for the 5% double-doped materials are very close to one another whereas

LaNb12.5 and LaNb2.5 exhibit higher values. The H^0 's for the trivalent (La10, Y10) and pentavalent (Nb10) doped materials are similar to that of pure ceria. This result is not surprising, given that singly trivalent and pentavalent dopants are expected to behave similarly to ceria.^{17,30,46,47} The trends for the partial molar entropy are very similar to those of the partial molar enthalpy and are shown in Fig. 8b. S^0 of the double doped materials is slightly higher than Hf10 whereas S^0 of the trivalent and pentavalent single doped materials is in the order of pure ceria. For all investigated materials, S^0 decreases with

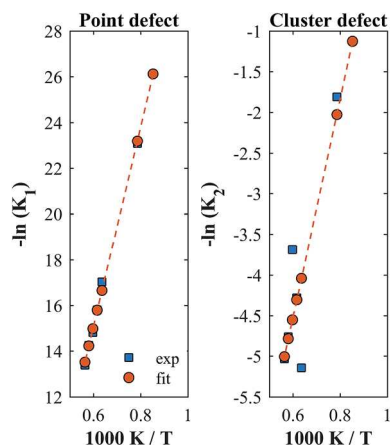


Fig. 6 Equilibrium constants for YNb5. The squares are isothermally derived values, the dots are based on a linear fit in the Van't Hoff plot.

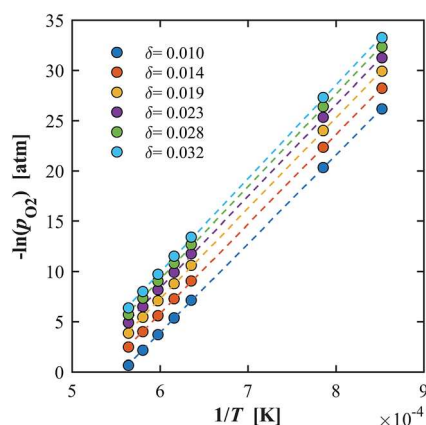


Fig. 7 Van't Hoff plot for YNb5 showing the linear correlation between $-\ln(p_{O_2})$ and $1/T$ for $\delta = 0.01$ – 0.032 . Constant δ values were calculated for T in the range 1173–1773 K.

increasing reduction extent. A comparison of the partial molar enthalpy and entropy calculated in this work to literature values for pure and Zr doped ceria at $\delta = 0.012$ is shown in Table 4.

Table 4 Partial molar enthalpy and entropy for $\delta = 0.012$ calculated in this work and literature values for pure and Zr doped ceria

	ΔH^0 [kJ mol ⁻¹]	ΔS^0 [J mol ⁻¹ K ⁻¹]
CeO ₂ (this work)	444	234
CeO ₂ (Panlener) ³⁷	467	251
Zr5 (Takacs) ¹³	407	226
Hf10	360 ^a	200 ^a
Nb10	436	228
Y10	444 ^b	231 ^b
La10	449	236
YNb5	368	201
ScNb5	372	207
LaNb5	366	192
LaNb2.5	395	213
LaNb12.5	386	202

^a Values taken at $\delta = 0.015$. ^b Values taken at $\delta = 0.010$.

In general, thermodynamic data in the high temperature range relevant for solar thermochemical gas splitting remain scarce and most partial molar properties are extracted from nonstoichiometry data at lower temperatures.^{12,37,40,46,48} However, we found that the temperature range of the evaluated data has a large influence on the calculated H^0 . In the case of pure ceria, the slope of the derived partial molar enthalpy varies significantly when calculated based on the temperature ranges of 1273–1773 K or 1573–1773 K, as seen in Fig. 9. This is true not only for the experimental data gathered in this work but also for data extracted from Panlener *et al.*,³⁷ which indicates the sensitivity of the slope of a constant δ line in the Van't Hoff plot when there are few data points for the linear regression. The beneficial influence of a wider temperature range on the extracted thermodynamic properties was also pointed out by Bork *et al.*⁴⁹ who uses a database including a wide range of literature data to obtain a higher statistically accuracy.

3.4 Efficiency

The above determined partial molar properties were used to calculate the $\eta_{\text{solar-to-fuel}}$ of the PCCD materials. Zr5 (ref. 13) and

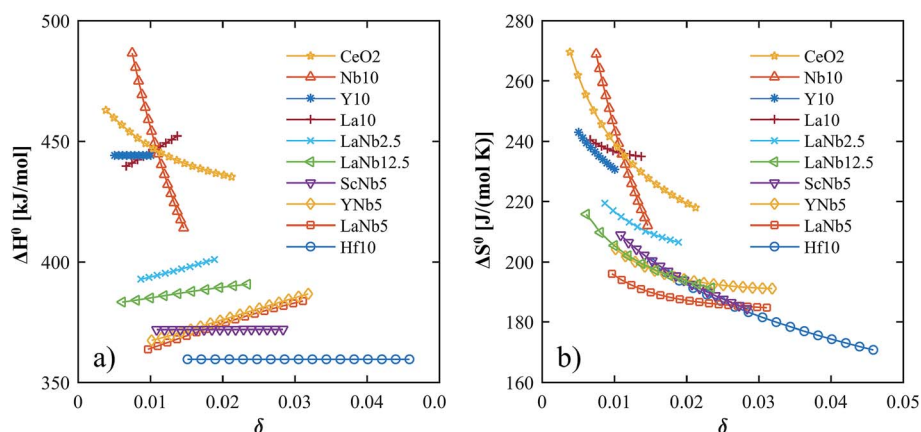


Fig. 8 Partial molar enthalpy (a) and entropy (b) as a function of the nonstoichiometry for all investigated materials.



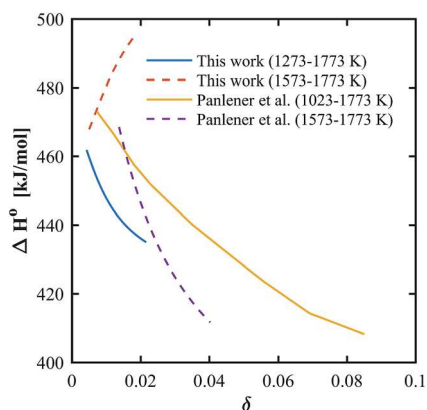


Fig. 9 Partial molar enthalpy for pure ceria based on experimental data in different temperature ranges, using experimental data from this work and experimental data from Panlener *et al.*³⁷

pure ceria³⁷ were included as references. Fig. 10 shows $\eta_{\text{solar-to-fuel}}$ as a function of the temperature swing between reduction and oxidation. The PCCD materials reach a maximum $\eta_{\text{solar-to-fuel}}$ in the range 22–31% for a temperature swing between the reduction and oxidation steps of $\Delta T = 200$ –300 K for H_2O and $\Delta T = 250$ –400 K for CO_2 . An optimal temperature arises because the energy demand for steam evaporation and CO_2 separation dominate at lower temperature swings while the energy requirements for heating of the solids dominate at larger temperature swings. YNb5 reaches the highest $\eta_{\text{solar-to-fuel}}$ of 31% and 28% for H_2 and CO production, respectively, compared to 26% and 24% achieved by undoped ceria and 29% and 26% by Zr doped ceria. The optimal temperature swings for the PCCD materials are between those of Zr-doped and undoped ceria as their reduction enthalpies are between that of Zr and pure ceria. Values of $\eta_{\text{solar-to-fuel}}$ for undoped ceria based on our calculated partial molar properties are in good agreement with those using thermodynamic values from literature.³⁷ $\eta_{\text{solar-to-fuel}}$ for all investigated materials is shown in Fig. S6.†

4. Conclusions

We fabricated, characterized, and experimentally determined the thermodynamic properties of paired charge-compensating doped ceria (PCCD), namely: ScNb5, YNb5, LaNb2.5, LaNb5, and LaNb12.5. We further compared their redox performance to single doped Y10, La10, Nb10, and Hf10. We found that the PCCD materials are phase pure and stable over multiple redox cycles. Their partial molar reduction enthalpies are between those of Hf doped ceria and pure ceria, and the values are sensitive to the temperature range in which the non-stoichiometry data is evaluated. By using a wide range of temperatures and pressures, we achieved a good match between the predicted and experimentally determined non-stoichiometries. A system efficiency model indicated that PCCD materials can improve the redox performance of ceria, in contrast to doping with the individual components. PCCD materials require smaller temperature swings between reduction and oxidation than Zr doped ceria. The highest solar-to-fuel energy conversion efficiency was obtained by YNb5 for a reduction temperature of 1773 K and oxidation temperatures of 1473–1523 K. Overall, this analysis shows that the PCCD materials are promising for solar thermochemical redox cycles.

Conflicts of interest

The authors declare no conflicts of interest.

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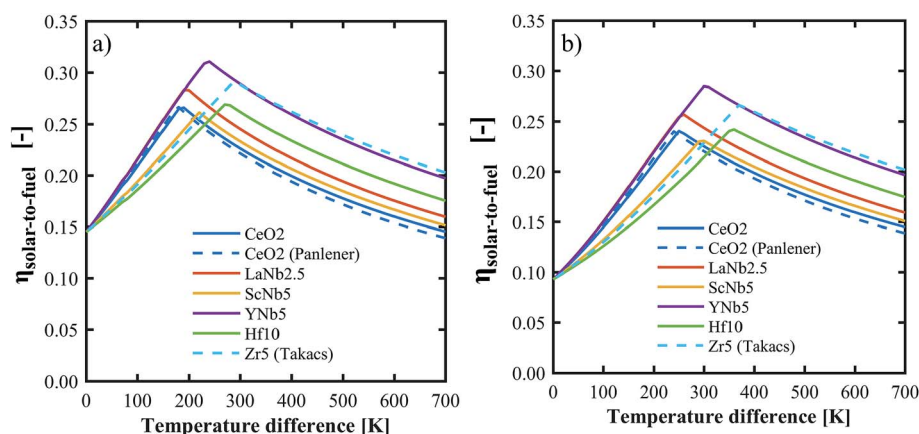


Fig. 10 Solar-to-fuel energy conversion efficiency for the production of H_2 (a) and CO (b) as a function of the temperature swing between reduction and oxidation. Thermodynamic data for CeO_2 and Zr5 are from ref. 37 and 13 respectively. System parameters are listed in Table 1.



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